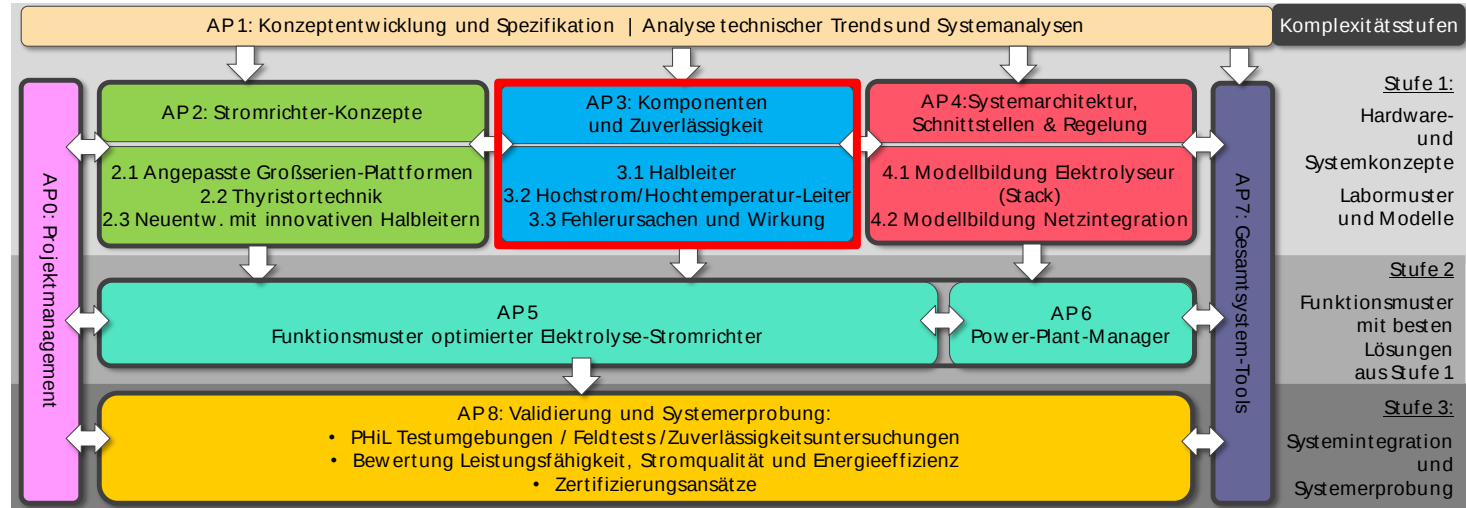




Optimized Semiconductor Power Modules for Electrolyzer System Applications

Varun Raghunath | 26 September 2025

Overview Infineon Work packages

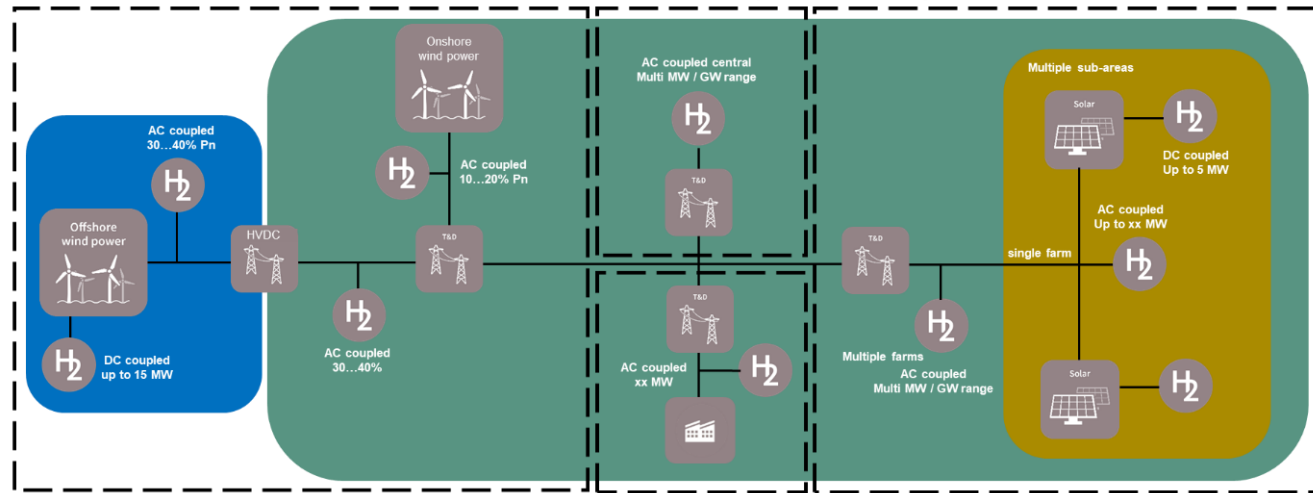


▮ Collaboration in AP 0, AP 1, AP 2 und AP 8

▮ Focus on AP 3.1 Semiconductors

AP 2 Power converter concepts and application landscape from Infineon perspective

Electrolysis with co-located windfarm



Co-located with large consumers

- ▮ Diverse in terms of
- ▮ Location
- ▮ Output voltage level/type
- ▮ Operating mode
- ▮ Source: own illustration

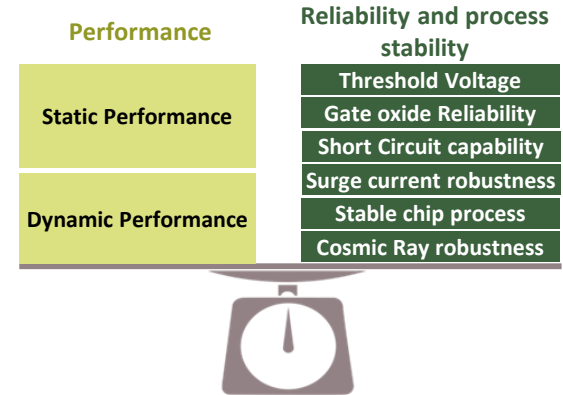
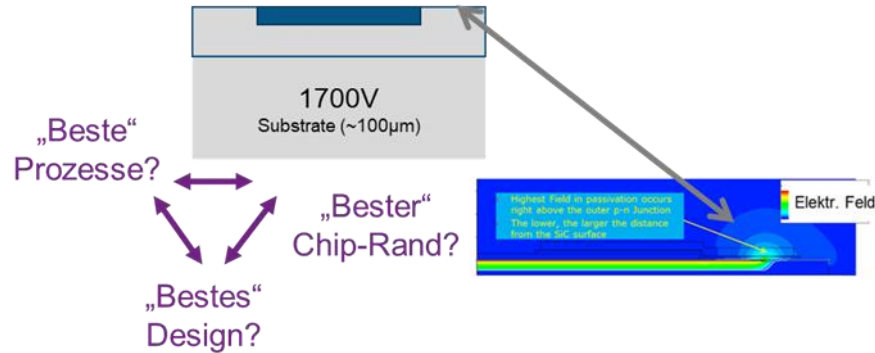
AP 3.1.1 Semiconductor technologies

Comparison between Si and SiC material parameters

Material Parameter	Si	SiC	Effects for SiC (at same voltage /current)	Required adaptations for SiC module
Bandgap (eV)	1,1	3,3	+ Smaller chips + Better switching losses - Higher electric field at chip edges	Innovative solution for edge termination
Thermal conductivity (W/mK)	150	490	- Higher thermal gradients on the back of the chip	Change from solder to sinter connection technology
Heat dissipation coefficient (ppm/K)	2,3	3,5	- Higher load through thermal expansion	New requirement for interconnect technologies
Youngs Modulus (GPa)	130	450	- Higher load through higher stiffness	New requirement for interconnect technologies

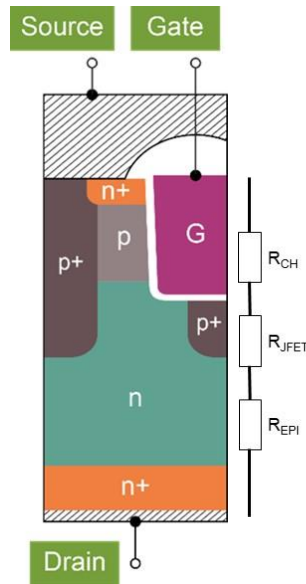
AP 3.1.1: Semiconductor technologies

Fundamental considerations



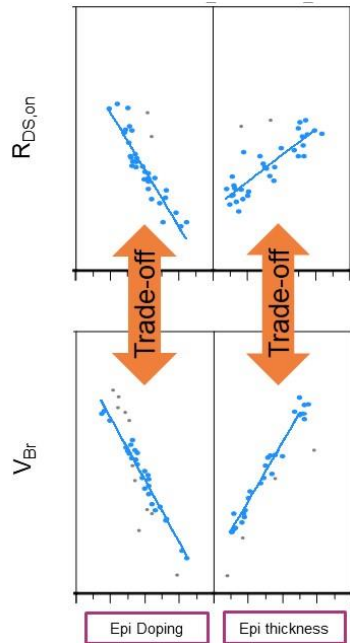
- ▮ Adaptation of >100 individual processes to achieve a reliable design point
- ▮ Electrical fields at the chip edge are significantly higher than with Si
 - ▮ Avoidance of field peaks
 - ▮ Examination of the passivation (chip and module)

AP 3.1.1: SiC MOSFET – fundamental design trade-offs



- ▮ Channel resistance R_{CH} can be optimized through the front end processes
- ▮ JFET resistance R_{JFET} can be adjusted by optimizing the doping
- ▮ Drift zone resistance R_{EPI} can be adjusted with the thickness of the epitaxial layer and the doping
 - ▮ This has direct effect on the blocking voltage
 - ▮ Electrical field at the gate oxide
 - ▮ Robustness against cosmic radiation

AP 3.1.1: Front end tests – focus on $R_{DS,ON}$ and V_{Br}

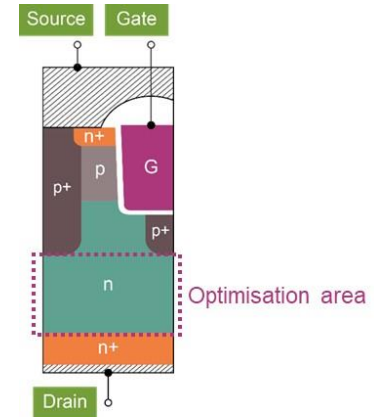
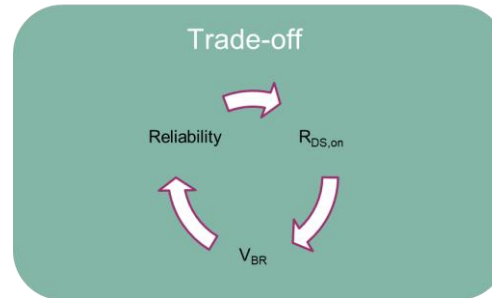


Result for $R_{DS,ON}$

Higher dependence on doping of the drift zone

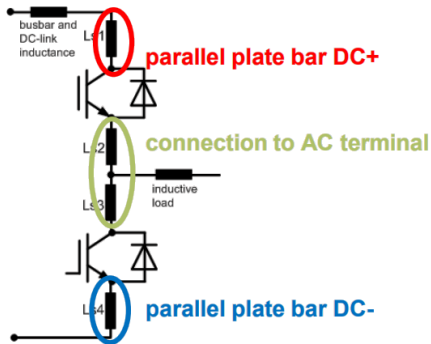
Result for V_{Br}

High dependence on doping and thickness of the drift zone

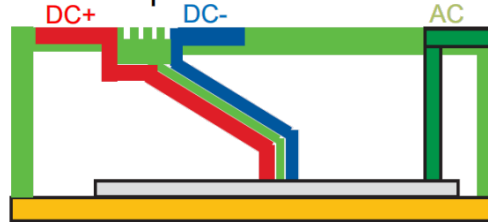


AP 3.1.2: Module for hybrid thyristor topologies

- ▢ Intensive discussion with SMA and TUD
 - ▢ First indications of voltages >1.5kVDC (up to 2kVDC)
 - ▢ Considerations for a high current 2.3kV and 3.3kV SiC MOSFET module



Strip line concept



XHP™ 2

HyLeiT AP 3.1.2 Sample modules

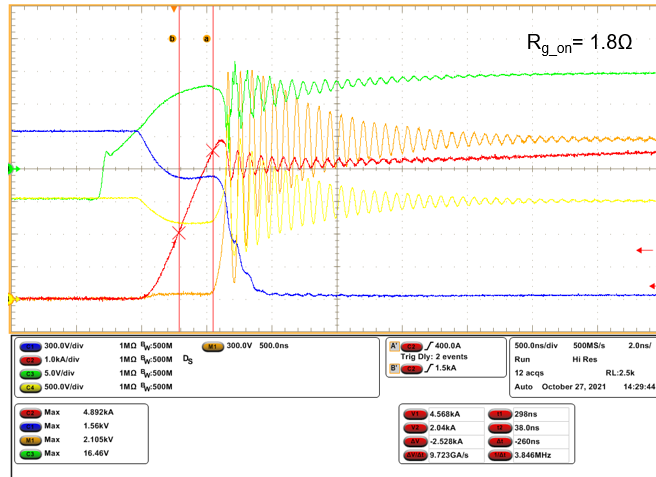
$R_{DS,ON} = 1\text{m}\Omega @ 25^\circ\text{C}$

$I_{NOM} = 2000\text{ A}$

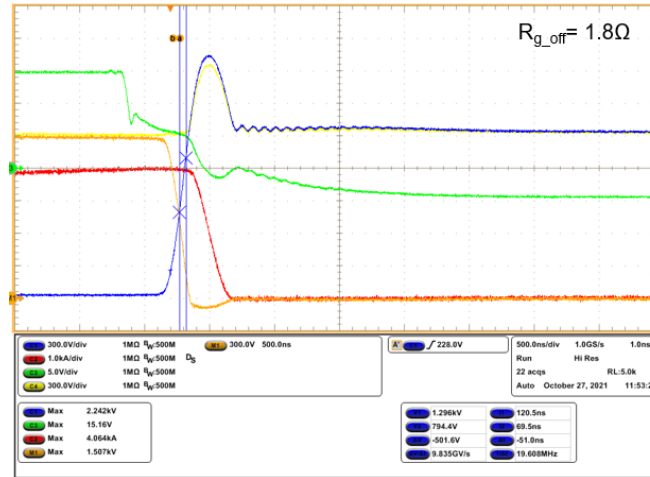
AP 3.1.2: Characterization of module

Switching curves 1.5 kV / 2x I_{nom} / 150°C (early prototypes)

Turn ON



Turn OFF



Low side

Ch1 (Blue): U_{DS}

Ch2 (Red): I_D

Ch3 (Green): U_{GS}

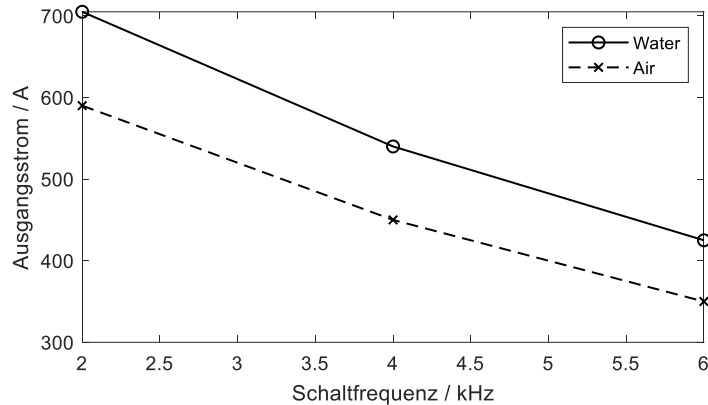
High side

M1 (Orange): $U_{DS, \text{Bodydiode}}$

AP 3.1.2: Scaling and simulating in application

Performance estimation HyLeiT-Module

Output current vs switching frequency



$U_{DC} = 1.2 \text{ kV}$
 $U_{OUT} = 800 \text{ V}$
 $f_{SW} = 2 \dots 6 \text{ kHz}$

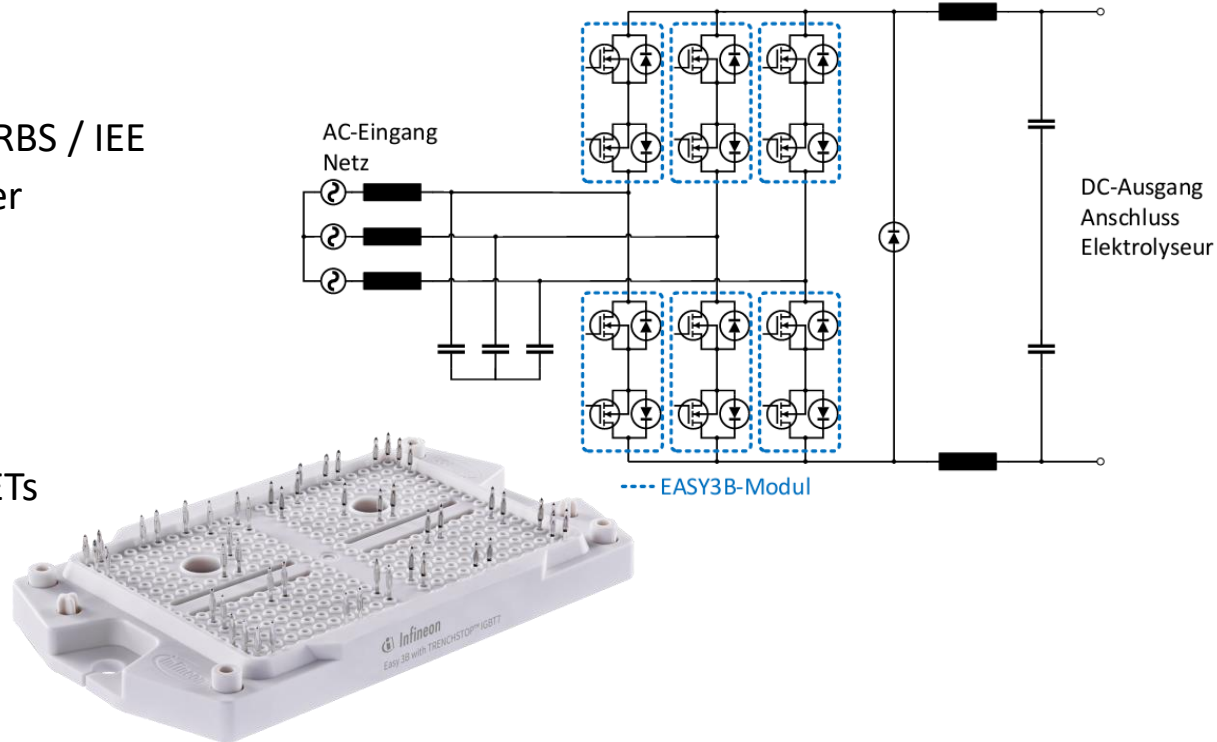


Number of required modules (28 kA)

Liquid cooling: 40 – 65 (17 K/kW)
 Forced air cooling: 48 – 80 (50 K/kW)

AP 3.1.3: Module for innovative rectifier

- ▢ Topology decision from H-RBS / IEE
 - ▢ Six switch buck converter
- ▢ 1200V SiC MOSFET
- ▢ Easy 3B package
 - ▢ Common source MOSFETs





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Thank you

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